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(54) Title: A GOLF CLUB HEAD WITH A FACE COMPOSED OF A FORGED MATERIAL

(57) Abstract: A golf club (40) having a club head (42) with a striking plate (72) having a thickness in the range of 0.010 to 0.250 inch is disclosed herein. The club head (42) may be composed of three pieces, a face (60), a sole (64) and a crown (64). Each of the pieces (60, 62 and 64) may be composed of a titanium material. The striking plate (72) of the club head (42) may have an aspect ratio less than 1.7. The striking plate (72) may also have concentric regions of thickness with the thickness portion in the center. The club head (42) may be composed of a titanium material, have a volume in the range of 175 cubic centimeters to 400 cubic centimeters, a weight in the range of 165 grams to 300 grams, and a striking plate (72) surface area in the range of 4.00 square inches to 7.50 square inches. The golf club head (42) may also have a coefficient of restitution greater than 0.8 under test conditions such as the USGA test conditions specified pursuant to Rule 4-1e, Appendix II, of the Rules of Golf for 1998-1999.

Title

A GOLF CLUB HEAD WITH A FACE COMPOSED OF A FORGED MATERIAL

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Technical Field

The present invention relates to a golf club head with a face composed of a forged material. More specifically, the present invention relates to a golf club head with face composed of a thin forged material for a more efficient transfer energy to a golf ball at impact.

10

Background Art

When a golf club head strikes a golf ball, large impacts are produced that load the club head face and the golf ball. Most of the energy is transferred from the head to the golf ball, however, some energy is lost as a result of the collision. The golf ball is typically composed of polymer cover materials (such as ionomers) surrounding a rubber-like core. These softer polymer materials having damping (loss) properties that are strain and strain rate dependent which are on the order of 10-100 times larger than the damping properties of a metallic club face. Thus, during impact most of the energy is lost as a result of the high stresses and deformations of the golf ball (0.001 to 0.20 inches), as opposed to the small deformations of the metallic club face (0.025 to 0.050 inches). A more efficient energy transfer from the club head to the golf ball could lead to greater flight distances of the golf ball.

15

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The generally accepted approach has been to increase the stiffness of the club head face to reduce metal or club head deformations. However, this leads to greater

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deformations in the golf ball, and thus increases in the energy transfer problem.

Some have recognized the problem and disclosed possible solutions. An example is Campau, U.S. Patent Number 4,398,965, for a Method Of Making Iron Golf Clubs With Flexible Impact Surface, which discloses a club having a flexible and resilient face plate with a slot to allow for the flexing of the face plate. The face plate of Campau is composed of a ferrous material, such as stainless steel, and has a thickness in the range of 0.1 inches to 0.125 inches.

Another example is Eggiman, U.S. Patent Number 5,863,261, for a Golf Club Head With Elastically Deforming Face And Back Plates, which discloses the use of a plurality of plates that act in concert to create a spring-like effect on a golf ball during impact. A fluid is disposed between at least two of the plates to act as a viscous coupler.

Yet another example is Jepson et al, U.S. Patent Number 3,937,474, for a golf Club With A Polyurethane Insert. Jepson discloses that the polyurethane insert has a hardness between 40 and 75 shore D.

Still another example is Inamori, U.S. Patent Number 3,975,023, for a Golf Club Head With Ceramic Face Plate, which discloses using a face plate composed of a ceramic material having a high energy transfer coefficient, although ceramics are usually harder materials. Chen et al., U.S Patent Number 5,743,813 for a Golf Club Head, discloses using multiple layers in the face to absorb the shock of the golf ball. One of the materials is a non-metal material.

Lu, U.S. Patent Number 5,499,814, for a Hollow Club Head With Deflecting Insert Face Plate, discloses a reinforcing element composed of a plastic or aluminum alloy that allows for minor deflecting of the face plate which has a thickness ranging from 0.01 to 0.30 inches for a variety of materials including stainless steel, titanium, 5 KEVLAR®, and the like. Yet another Campau invention, U.S. Patent Number 3,989,248, for a Golf Club Having Insert Capable Of Elastic Flexing, discloses a wood club composed of wood with a metal insert.

Although not intended for flexing of the face plate, Viste, U.S. Patent Number 5,282,624 discloses a golf club head having a face plate composed of a forged stainless 10 steel material and having a thickness of 3 mm. Anderson, U.S. Patent Number 5,344,140, for a Golf Club Head And Method Of Forming Same, also discloses use of a forged material for the face plate. The face plate of Anderson may be composed of several forged materials including steel, copper and titanium. The forged plate has a uniform thickness of between 0.090 and 0.130 inches.

15 Another invention directed toward forged materials in a club head is Su et al., U.S. Patent Number 5,776,011 for a Golf Club Head. Su discloses a club head composed of three pieces with each piece composed of a forged material. The main objective of Su is to produce a club head with greater loft angle accuracy and reduce structural weaknesses. Finally, Aizawa, U.S. Patent Number 5,346,216 for a Golf 20 Club Head, discloses a face plate having a curved ball hitting surface.

The Rules of Golf, established and interpreted by the United States Golf

Association ("USGA") and The Royal and Ancient Golf Club of Saint Andrews, set forth certain requirements for a golf club head. The requirements for a golf club head are found in Rule 4 and Appendix II. A complete description of the Rules of Golf are available on the USGA web page at www.usga.org. Although the Rules of Golf do not

5 expressly state specific parameters for a golf club face, Rule 4-1e prohibits the face from having the effect at impact of a spring with a golf ball. In 1998, the USGA adopted a test procedure pursuant to Rule 4-1e, which measures club face COR. This USGA test procedure, as well as procedures like it, may be used to measure club face COR.

10 Although the prior art has disclosed many variations of face plates, the prior art has failed to provide a face plate with a high coefficient of restitution composed of a thin material.

Summary of the Invention

15 The present invention provides a golf club head with a striking plate having a high coefficient of restitution in order to increase the post-impact velocity of a golf ball for a given pre-impact club head velocity. The present invention is able to accomplish this by using a striking plate composed of a thin material, having a small aspect ratio (near 1.0) and having a large surface area.

20 One aspect of the present invention is a golf club head having a striking plate having a thickness in the range of 0.010 inches to 0.250 inches, and having a coefficient

of restitution of at least 0.83 under test conditions, such as those specified by the USGA. The standard USGA conditions for measuring the coefficient of restitution is set forth in the *USGA Procedure for Measuring the Velocity Ratio of a Club Head for Conformance to Rule 4-1e, Appendix II. Revision I, August 4, 1998 and Revision 0, July 6, 1998*, available from the USGA.

Another aspect of the present invention is a golf club head including a face member, a crown and a sole. The face member is composed of a material selected from titanium, titanium alloys, steels, vitreous metals, composites and ceramics. The face member includes a striking plate for striking a golf ball, a face extension and an interior tubing. The face extension extends laterally inward from a perimeter of the striking plate. The interior tubing receives a shaft and engages an upper portion of the face extension and a lower portion of the face extension. The crown is secured to the upper portion of the face extension at a varying distance from the striking plate. The sole plate is secured to the lower portion of the face extension at a varying distance from the striking plate.

Yet another aspect of the present invention is a golf club head having a striking plate with an aspect ratio no greater than 1.7. The aspect ratio is the ratio of width of the face to the height of the face. Normally, the aspect ratios of club head faces are relatively greater than 1.7. For example, the aspect ratio of the original GREAT BIG BERTHA® driver from Callaway Golf Company of Carlsbad, California was 1.9. As described in greater detail below, the smaller aspect ratio of the striking plate of the

club head of the present invention allows for greater compliance and thus a larger coefficient of restitution.

Yet another aspect of the present invention is a golf club head including a body composed of a titanium material and having a volume in the range of 175 cubic centimeters to 400 cubic centimeters, and preferably 260 cubic centimeters to 350 cubic centimeters, and most preferably in the range of 300 cubic centimeters to 310 cubic centimeters, a weight in the range of 160 grams to 300 grams, preferably 175 grams to 225 grams, and a face having a surface area in the range of 4.50 square inches to 5.50 square inches, and preferably in the range of 4.00 square inches to 7.50 square inches.

10

Brief Description of the Drawings

FIG. 1 is a front view of the golf club of the present invention.

FIG. 1A is a front view of an alternative embodiment of the golf club of the present invention.

15 FIG. 2 is a top plan view of golf club head of FIG. 1.

FIG. 2A is a top plan view of an alternative embodiment of the golf club of the present invention.

FIG. 3 is a top plan isolated view of the face member of the golf club head of the present invention with the crown in phantom lines.

20 FIG. 4 is a side plan view of the golf club head of the present invention.

FIG. 4A is a side plan view of an alternative embodiment of the golf club head

of the present invention.

FIG. 5 is a bottom view of the golf club head of the present invention.

FIG. 6 is a cross-sectional view along line 6-6 of FIG. 5.

FIG. 7 is a cross-sectional view along line 7-7 of FIG. 3 illustrating the hosel of
5 the golf club head present invention.

FIG. 8 is an enlarged view of circle 8 of FIG. 7.

FIG. 9 is a top plan view of overlaid embodiments of the face member of the
golf club head of the present invention.

FIG. 10 is a side view of overlaid embodiments of the face member of the golf
10 club head of the present invention.

FIG. 11 is a bottom plan view of overlaid embodiments of the face member of
the golf club head of the present invention.

FIG. 12 is a front view of the golf club head of the present invention illustrating
the variations in thickness of the striking plate.

15 FIG. 12A is a front view of an alternative golf club head of the present invention
illustrating the variations in thickness of the striking plate.

FIG. 13 is a cross-sectional view along line 13-13 of FIG. 12 showing face
thickness variation.

FIG. 14 is a front plan view of a BIG BERTHA® WARBIRD® driver of the
20 prior art.

FIG. 15 is a perspective view of a face centered cubic model.

FIG. 16 is a perspective view of a body centered cubic model.

FIG. 17 is a side view of a golf club head of the present invention immediately prior to impact with a golf ball.

FIG. 18 is a side view of a golf club head of the present invention during impact
5 with a golf ball.

FIG. 19 is a side view of a golf club head of the present invention immediately after impact with a golf ball.

FIG. 20 is a graph of the percentage change in von Mises stresses using a GREAT BIG BERTHA® shaped golf club as a base reference versus Area for the face
10 center, the face sole and the face crown of the golf club head of the present invention.

FIG. 21 is a graph of the percentage change in COR and Face Deflection using a GREAT BIG BERTHA® shaped golf club as a base reference versus Area.

FIG. 22 is a graph of the percentage change in von Mises stresses using a GREAT BIG BERTHA® shaped golf club as a base reference versus Aspect ratio for
15 the face center, the face sole and the face crown of the golf club head of the present invention.

FIG. 23 is a graph of the percentage change in COR and Face Deflection using a GREAT BIG BERTHA® shaped golf club as a base reference versus Aspect ratio.

FIG. 24 is a graph of the percentage change in von Mises stresses using a
20 GREAT BIG BERTHA® shaped golf club as a base reference versus Thickness ratio for the face center, the face sole and the face crown of the golf club head of the present

invention.-

FIG. 25 is a graph of the percentage change in COR and Face Deflection using a GREAT BIG BERTHA® shaped golf club as a base reference versus Thickness ratio.

FIG. 26 is a graph of the percentage change in COR using a GREAT BIG BERTHA® shaped golf club as a base reference versus the percentage change in Face deflection using a GREAT BIG BERTHA® shaped golf club as a base reference for the aspect ratio, the area and thickness ratio of a golf club of the present invention.

FIG. 27 is a graph of the percentage change in COR using a GREAT BIG BERTHA® shaped golf club as a base reference versus the percentage change in Face crown von Mises stress using a GREAT BIG BERTHA® shaped golf club as a base reference for the aspect ratio, the area and thickness ratio of a golf club of the present invention.

FIG. 28 is a graph of the percentage change in COR using a GREAT BIG BERTHA® shaped golf club as a base reference versus the percentage change in Face center von Mises stress using a GREAT BIG BERTHA® shaped golf club as a base reference for the aspect ratio, the area and thickness ratio of a golf club of the present invention.

FIG. 29 is a graph of the percentage change in COR using a GREAT BIG BERTHA® shaped golf club as a base reference versus the percentage change in Face sole von Mises stress using a GREAT BIG BERTHA® shaped golf club as a base reference for the aspect ratio, the area and thickness ratio of a golf club.

Best Mode(s) For Carrying Out The Invention

The present invention is directed at a golf club head having a striking plate that is thin and has a high coefficient of restitution thereby enabling for greater distance of a golf ball hit with the golf club head of the present invention. The coefficient of
5 restitution (also referred to herein as "COR") is determined by the following equation:

$$e = \frac{v_2 - v_1}{U_1 - U_2}$$

wherein U_1 is the club head velocity prior to impact; U_2 is the golf ball velocity prior
10 to impact which is zero; v_1 is the club head velocity just after separation of the golf ball from the face of the club head; v_2 is the golf ball velocity just after separation of the golf ball from the face of the club head; and e is the coefficient of restitution between the golf ball and the club face.

The values of e are limited between zero and 1.0 for systems with no energy addition.
15 The coefficient of restitution, e , for a material such as a soft clay or putty would be near zero, while for a perfectly elastic material, where no energy is lost as a result of deformation, the value of e would be 1.0. The present invention provides a club head having a striking plate or face with a coefficient of restitution approaching 0.93, as measured under conventional test conditions.

20 As shown in FIGS. 1-5, a golf club is generally designated 40. The golf club 40 has a golf club head 42 with a body 44 and a hollow interior, not shown. Engaging the club head 42 is a shaft 48 that has a grip 50, not shown, at a butt end 52 and is inserted

into a hosel 54 at a tip end 56. An O-ring 58 may encircle the shaft 48 at an aperture 59 to the hosel 54.

The body 44 of the club head 42 is generally composed of three sections, a face member 60, a crown 62 and a sole 64. The club head 42 may also be partitioned into a heel section 66 nearest the shaft 48, a toe section 68 opposite the heel section 66, and a rear section 70 opposite the face member 60.

The face member 60 is generally composed of a single piece of metal, and is preferably composed of a forged metal material. More preferably, the forged metal material is a forged titanium material. However, those skilled in the relevant art will recognize that the face member may be composed of other materials such as steels, vitreous metals, ceramics, composites, carbon, carbon fibers and other fibrous materials without departing from the scope and spirit of the present invention. The face member 60 generally includes a face plate (also referred to herein as a striking plate) 72 and a face extension 74 extending laterally inward from the perimeter of the face plate 72. The face plate 72 has a plurality of scorelines 75 thereon. An alternative embodiment of the face plate 72 is illustrated in FIG. 1A which has a different scoreline pattern. The face extension 74 generally includes an upper lateral extension 76, a lower lateral extension 78, a heel wall 80 and a toe wall 82.

The upper lateral extension 76 extends inward, toward the hollow interior 46, a predetermined distance to engage the crown 62. In a preferred embodiment, the predetermined distance ranges from 0.2 inches to 1.0 inches, as measured from the

perimeter 73 of the face plate 72 to the edge of the upper lateral extension 76. Unlike the prior art which has the crown engage the face plate perpendicularly, the present invention has the face member 60 engage the crown 62 along a substantially horizontal plane. Such engagement enhances the flexibility of the face plate 72 allowing for a greater coefficient of restitution. The crown 62 and the upper lateral extension 76 are secured to each other through welding or the like along the engagement line 81. As illustrated in FIG. 2A, in an alternative embodiment, the upper lateral extension 76 engages the crown 62 at a greater distance inward thereby resulting in a weld that is more rearward from the stresses of the face plate 72 than that of the embodiment of

10 FIG. 2.

The uniqueness of the present invention is further demonstrated by a hosel section 84 of the face extension 74 that encompasses the aperture 59 leading to the hosel 54. The hosel section 84 has a width w_1 that is greater than a width w_2 of the entirety of the upper lateral extension 76. The hosel section 84 gradually transitions

15 into the heel wall 80. The heel wall 80 is substantially perpendicular to the face plate 72, and the heel wall 80 covers the hosel 54 before engaging a ribbon 90 and a bottom section 91 of the sole 64. The heel wall 80 is secured to the sole 64, both the ribbon 90 and the bottom section 91, through welding or the like.

At the other end of the face member 60 is the toe wall 82 which arcs from the

20 face plate 72 in a convex manner. The toe wall 82 is secured to the sole 64, both the ribbon 90 and the bottom section 91, through welding or the like.

The lower lateral extension 78 extends inward, toward the hollow interior 46, a predetermined distance to engage the sole 64. In a preferred embodiment, the predetermined distance ranges from 0.2 inches to 1.0 inches, as measured from the perimeter 73 of the face plate 72 to the end of the lower lateral extension 78. Unlike
5 the prior art which has the sole plate engage the face plate perpendicularly, the present invention has the face member 60 engage the sole 64 along a substantially horizontal plane. This engagement moves the weld heat affected zone rearward from a strength critical crown/face plate radius region. Such engagement enhances the flexibility of the face plate 72 allowing for a greater coefficient of restitution. The sole 64 and the lower
10 lateral extension 78 are secured to each other through welding or the like, along the engagement line 81. The uniqueness of the present invention is further demonstrated by a bore section 86 of the face extension 74 that encompasses a bore 114 in the sole 64 leading to the hosel 54. The bore section 86 has a width w_3 that is greater than a width w_4 of the entirety of the lower lateral extension 78. The bore section 86 gradually
15 transitions into the heel wall 80.

The crown 62 is generally convex toward the sole 64, and engages the ribbon 90 of sole 64 outside of the engagement with the face member 60. The crown 62 may have a chevron decal 88, or some other form of indicia scribed therein that may assist in alignment of the club head 42 with a golf ball. The crown 62 preferably has a thickness
20 in the range of 0.025 to 0.060 inches, and more preferably in the range of 0.035 to 0.043 inches, and most preferably has a thickness of 0.039 inches. The crown 62 is

preferably composed of a hot formed or "coined" material such as a sheet titanium.

However, those skilled in the pertinent art will recognize that other materials or forming processes may be utilized for the crown 62 without departing from the scope and spirit of the present invention.

5 The sole 64 is generally composed of the bottom section 91 and the ribbon 90 which is substantially perpendicular to the bottom section 91. The bottom section 91 is generally convex toward the crown 62. The bottom section has a medial ridge 92 with a first lateral extension 94 toward the toe section 68 and a second lateral extension 96 toward the heel section 66. The medial ridge 92 and the first lateral extension 94 define
10 a first convex depression 98, and the medial ridge 92 and the second lateral extension 96 define a second convex depression 100. The sole 64 preferably has a thickness in the range of 0.025 to 0.060 inches, and more preferably 0.047 to 0.055 inches, and most preferably has a thickness of 0.051 inches. The sole 64 is preferably composed of a hot formed or "coined" metal material such as a sheet titanium material. However, those
15 skilled in the pertinent art will recognize that other materials and forming processes may be utilized for the sole 64 without departing from the scope and spirit of the present invention.

FIGS. 6-8 illustrate the hollow interior 46 of the club head 42 of the present invention. The hosel 54 is disposed within the hollow interior 46, and is located as a
20 component of the face member 60. The hosel 54 may be composed of a similar material to the face member 60, and is secured to the face member 60 through welding

or the like. The hosel 54 is located in the face member 60 to concentrate the weight of the hosel 54 toward the face plate 72, near the heel section 66 in order to contribute to the ball striking mass of the face plate 72. A hollow interior 118 of the hosel 54 is defined by a hosel wall 120 that forms a cylindrical tube between the bore 114 and the aperture 59. In a preferred embodiment, the hosel wall 120 does not engage the heel wall 80 thereby leaving a void 115 between the hosel wall 120 and the heel wall 80. The shaft 48 is disposed within the hosel 54. Further, the hosel 54 is located rearward from the face plate 72 in order to allow for compliance of the face plate 72 during impact with a golf ball. In one embodiment, the hosel 54 is disposed 0.125 inches rearward from the face plate 72.

Optional dual weighting members 122 and 123 may also be disposed within the hollow interior 46 of the club head 42. In a preferred embodiment, the weighting members 122 and 123 are disposed on the sole 64 in order to lower the center of gravity of the golf club 40. The weighting members 122 and 123, not shown, may have a shape configured to the contour of the sole 64. However, those skilled in the pertinent art will recognize that the weighting member may be placed in other locations of the club head 42 in order to influence the center of gravity, moment of inertia, or other inherent properties of the golf club 40. The weighting members 122 and 123 are preferably a pressed and sintered powder metal material such as a powder titanium material. Alternatively, the weighting members 122 and 123 may be cast or machined titanium chips. Yet further, the weighting members 122 and 123 may be a tungsten

screw threadingly engaging an aperture 124 of the sole 64. Although titanium and tungsten have been used as exemplary materials, those skilled in the pertinent art will recognize that other high density materials may be utilized as an optional weighting member without departing from the scope and spirit of the present invention.

5 FIGS. 9-11 illustrate variations in the engagement line 81a or 81b. The engagement line 81b illustrates a variation of the face extension 74 of the face member 60. The variation has the engagement line located rearward of the chevron 88. The engagement line 81b is the preferred engagement line.

 FIGS. 12, 12A and 13 illustrate embodiments of the present invention having a
10 variation in the thickness of the face plate 72. The face plate or striking plate 72 is partitioned into elliptical regions, each having a different thickness. A central elliptical region 102 preferably has the greatest thickness that ranges from 0.110 inches to 0.090 inches, preferably from 0.103 inches to 0.093 inches, and is most preferably 0.095 inches. A first concentric region 104 preferably has the next greatest thickness that
15 ranges from 0.097 inches to 0.082 inches, preferably from 0.090 inches to 0.082 inches, and is most preferably 0.086 inches. A second concentric region 106 preferably has the next greatest thickness that ranges from 0.094 inches to 0.070 inches, preferably from 0.078 inches to 0.070 inches, and is most preferably 0.074 inches. A third concentric region 108 preferably has the next greatest thickness that ranges from 0.090 inches to
20 0.07 inches. A periphery region 110 preferably has the next greatest thickness that ranges from 0.069 inches to 0.061 inches. The periphery region includes toe periphery

region 110a and heel periphery region 110b. The variation in the thickness of the face plate 72 allows for the greatest thickness to be distributed in the center 111 of the face plate 72 thereby enhancing the flexibility of the face plate 72 which corresponds to a greater coefficient of restitution.

5 In an alternative embodiment, the striking plate 72 is composed of a vitreous metal such as iron-boron, nickel-copper, nickel-zirconium, nickel-phosphorous, and the like. These vitreous metals allow for the striking plate 72 to have a thickness as thin as 0.055 inches. Preferably, the thinnest portions of such a vitreous metal striking plate would be in the periphery regions 110a and 110b, although the entire striking plate 72
10 of such a vitreous metal striking plate 72 could have a uniform thickness of 0.055 inches.

 Yet in further alternative embodiments, the striking plate 72 is composed of ceramics, composites or other metals. Further, the face plate or striking plate 72 may be an insert for a club head such as wood or iron. Additionally, the thinnest regions of
15 the striking plate 72 may be as low as 0.010 inches allowing for greater compliance and thus a higher coefficient of restitution.

 The coefficient of restitution of the club head 42 of the present invention under standard USGA test conditions with a given ball ranges from 0.80 to 0.93, preferably ranges from 0.83 to 0.883 and is most preferably 0.87. The microstructure of titanium
20 material of the face member 60 has a face center cubic ("FCC") microstructure as shown in FIG. 15, and a body center cubic ("BCC") microstructure as shown in FIG.

16. The FCC microstructure is associated with alpha-titanium, and the BCC microstructure is associated with beta-titanium.

Additionally, the face plate 72 of the present invention has a smaller aspect ratio than face plates of the prior art (one example of the prior art is shown in FIG. 14). The aspect ratio as used herein is defined as the width, "w", of the face divided by the height, "h", of the face, as shown in FIG. 1A. In one embodiment, the width w is 78 millimeters and the height h is 48 millimeters giving an aspect ratio of 1.635. In conventional golf club heads, the aspect ratio is usually much greater than 1. For example, the original GREAT BIG BERTHA® driver had an aspect ratio of 1.9. The face of the present invention has an aspect ratio that is no greater than 1.7. The aspect ratio of the present invention preferably ranges from 1.0 to 1.7. One embodiment has an aspect ratio of 1.3. The face of the present invention is more circular than faces of the prior art. The face area of the face plate 72 of the present invention ranges 4.00 square inches to 7.50 square inches, more preferably from 4.95 square inches to 5.1 square inches, and most preferably from 4.99 square inches to 5.06 square inches.

The club head 42 of the present invention also has a greater volume than a club head of the prior art while maintaining a weight that is substantially equivalent to that of the prior art. The volume of the club head 42 of the present invention ranges from 175 cubic centimeters to 400 cubic centimeters, and more preferably ranges from 300 cubic centimeters to 310 cubic centimeters. The weight of the club head 42 of the present invention ranges from 165 grams to 300 grams, preferably ranges from 175

grams to 225 grams, and most preferably from 188 grams to 195 grams. The depth of the club head from the face plate 72 to the rear section of the crown 62 preferably ranges from 3.606 inches to 3.741 inches. The height, "H", of the club head 42, as measured while in striking position, preferably ranges from 2.22 inches to 2.27 inches, and is most preferably 2.24 inches. The width, "W", of the club head 42 from the toe section 68 to the heel section 66 preferably ranges from 4.5 inches to 4.6 inches.

As shown in FIGS. 17-19, the flexibility of the face plate 72 allows for a greater coefficient of restitution. At FIG. 17, the face plate 72 is immediately prior to striking a golf ball 140. At FIG. 18, the face plate 72 is engaging the golf ball, and deformation of the golf ball 140 and face plate 72 is illustrated. At FIG. 19, the golf ball 140 has just been launched from the face plate 72.

The golf club 42 of the present invention was compared to a golf club head shaped similar to the original GREAT BIG BERTHA® driver to demonstrate how variations in the aspect ratio, thickness and area will effect the COR and stresses of the face plate 72. However, the GREAT BIG BERTHA® reference had a uniform face thickness of 0.110 inches which is thinner than the original GREAT BIG BERTHA® driver from Callaway Golf Company. The GREAT BIG BERTHA® reference had a COR value of 0.830 while the original GREAT BIG BERTHA® driver had a COR value of 0.788 under test conditions, such as the USGA test conditions specified pursuant to Rule 4-1e, Appendix II of the Rules of Golf for 1998-1999. For a one-hundred mph face center impact for the GREAT BIG BERTHA® reference, the peak

stresses were 40 kilopounds per square inch ("ksi") for the face-crown, 49 ksi for the face-sole and 29 ksi for the face-center. The face deflection for the GREAT BIG BERTHA® reference at one-hundred mph was 1.25mm. FIGS. 20-29 illustrate graphs related to these parameters using the GREAT BIG BERTHA® reference as a base. The

5 face-crown refers to the upper lateral extension 76, the face-sole refers to the lower lateral extension 78, and the face-center refers to the center of the face plate 72.

FIG. 20 illustrates the percent changes from the stresses on a GREAT BIG BERTHA® reference versus changes in the area of the face plate 72. As illustrated in the graph, as the area increases the stress on the face-crown increases, and as the area decreases the stress on the face-crown decreases. The stresses on the face-center and

10 the face-sole remain relatively constant as the area of the face plate 72 increases or decreases.

FIG. 21 illustrates how changes in the area will affect the COR and face deflection. Small changes in the area will greatly affect the deflection of the face plate

15 72 while changes to the COR, although relatively smaller percentage changes, are significantly greater in effect. Thus, as the area becomes larger, the face deflection will increase while the COR will increase slightly, but with a significant effect relative to the face deflection.

FIG. 22 illustrates the percent changes from the stresses on a GREAT BIG BERTHA® reference versus changes in the aspect ratio of the face plate 72. As the

20 aspect ratio of the face plate 72 becomes smaller or more circular, the stress on the face

sole greatly increases whereas the stress on the face-center and the face-crown only increases slightly as the aspect ratio decreases.

FIG. 23 illustrates how changes in the aspect ratio will affect the COR and face deflection. Small changes in the aspect ratio will greatly affect the deflection of the face plate 72 while changes to the COR, although relatively smaller percentage changes, are significantly greater in effect. Thus, as the aspect ratio becomes more circular, the face deflection will increase while the COR will increase slightly, but with a significant effect relative to the face deflection.

FIG. 24 illustrates the percent changes from the stresses on a GREAT BIG BERTHA® reference versus changes in the thickness ratio. The thickness ratio is defined as the ratio of the face plate 72 to the face thickness of the GREAT BIG BERTHA® reference which has a face thickness of 0.110 inches. As illustrated in the graph, small changes in the thickness ratio will have significant changes in the stress of the face-crown, the face-center and the face-sole.

FIG. 25 illustrates how changes in the thickness ratio will affect the COR and face deflection. Small changes in the thickness ratio will greatly affect the deflection of the face plate 72 while changes to the COR are significantly smaller in percentage changes.

FIG. 26 combines FIGS. 21, 23 and 25 to illustrate which changes give the greatest changes in COR for a given percentage change in the face deflection. As illustrated, changing the aspect ratio will give the greatest changes in COR without

substantial changes in the face deflection. However, the generic shape of a golf club head dictates that greater total change in COR can be practically achieved by changing the area of the face.

FIG. 27 combines the face-crown results of FIGS. 20, 22 and 24 to illustrate which changes give the greatest changes in COR relative to face-crown stress. As illustrated, changing the aspect ratio will give the greatest changes in COR with the least changes in the face-crown stress. However, changes in the area should be used to obtain the greater overall change in COR.

FIG. 28 combines the face-center results of FIGS. 20, 22 and 24 to illustrate which changes give the greatest changes in COR relative face-center stress. As illustrated, changing the area will give the greatest changes in COR with the least changes in the face-center stress.

FIG. 29 combines the face-sole results of FIGS. 20, 22 and 24 to illustrate which changes give the greatest changes in COR relative to the face-sole stress. Similar to the results for the face-center, changing the area will give the greatest changes in COR with the least changes in the face-sole stress.

The changes in the thickness ratio provide the least amount of changes in the COR relative to the aspect ratio and the area. However, the golf club head 42 of the present invention utilizes all three, the thickness ratio, the aspect ratio and the area to achieve a greater COR for a given golf ball under test conditions such as the USGA test conditions specified pursuant to Rule 4-1e, Appendix II of the Rules of Golf for 1998-

1999. Thus, unlike a spring, the present invention increases compliance of the face plate to reduce energy losses to the golf ball at impact, while not adding energy to the system.

Table One illustrates the durability of the striking plate 72 of the golf club head 42 of the present invention versus commercially available golf clubs including: BIIM driver from Bridgestone Sports of Tokyo, Japan; KATANA SWORD 1 driver from Katana Golf of Tokyo, Japan; KATANA SWORD 2 from Katana Golf of Tokyo, Japan; S-YARD .301NF from Daiwa-Seiko of Tokyo, Japan; S-YARD .301NF from Daiwa-Seiko of Tokyo, Japan; Mizuno 300S from Mizuno Golf of Tokyo, Japan; the BIGGEST BIG BERTHA® from Callaway Golf Company of Carlsbad, California; and the GREAT BIG BERTHA® HAWK EYE® driver Callaway Golf Company of Carlsbad, California. The first column lists the golf club heads. Column two lists the COR of each golf club head. Column three lists the number of impacts with a USGA conforming golf ball before failure of the striking plate of each golf club head. Column four lists the face center thickness for some of the golf club heads. As shown in Table One, no other golf club head has a COR of at least 0.85 and a durability to withstand 2000 impacts with a golf ball at a speed of 110 miles per hour. Although the KATANA SWORD1 has a COR over 0.85, its durability is not sufficient since it fails at approximately 1500 impacts. The BIIM driver has a durability over 2000 impacts, however, it has a COR under 0.850. The MIZUNO 300S has a durability of approximately 5000 impacts, however, it has a COR under 0.840.

Table One

Club	COR	Failure	Face Center Thickness
12°	.875	5000	0.095
11°	.870	5000	0.100
10°	.865	4500	0.105
9°	.855	3500	0.110
BIIM	.845	3500	0.106
Katana Sword-1	.855	1500	0.106
Katana Sword-2	.830	2000	-----
5-Yard .301NF	.830	1500	-----
5-Yard .301NF11	.835	4000	0.102
Mizuno 300S	.839	5000	0.118
BBB	.795	4500	-----
GB Hawk Eye	.789	4500	-----

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Durability is determined by subjecting the golf club to repeated impacts with a golf ball fired from an air cannon at 110 miles per hour ("MPH"). The golf club is immovably secured to a frame with the striking plate facing the air cannon. Golf balls are repeatedly shot from the air cannon at 110 MPH for impact with the center of the striking plate. The golf balls are PINNACLE GOLD® golf balls, which conform to the USGA golf ball standards. After each set of 500 impacts, the club heads are inspected for failure. The club heads are inspected for face cracking, bulge & roll deviation, face deformation and weld, joint and seam cracking. The face cracking is inspected through use of illumination of at least 140 foot candles to see if cracking is greater than 0.50 inch. Such a crack would indicate failure. Face deformation is determined by using a straight edge and feeler gauges to inspect for a deviation greater than 0.005 inch

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- anywhere on the face. The bulge & roll is determined by bulge & roll gauges to inspect for a deviation greater than 0.005 inch at the center of the face. The welds, joints and seams are inspected through use of illumination of at least 140 foot candles to see if there is any cracking between the surfaces. The most important factor is face cracking,
- 5 which will result in failure of a golf club if the crack is greater than 0.50 inch.

CLAIMS

1. A golf club comprising:
a golf club head having a striking plate, the golf club head a having a
5 coefficient of restitution of at least 0.85, and the striking plate having the durability to
withstand failure after at least 2000 impacts with an USGA conforming golf ball
against a center of the striking plate at approximately 110 miles per hour.
2. The golf club according to claim 1 wherein the striking plate has a thickness in
10 the range of 0.035 to 0.125.
3. The golf club according to claim 1 wherein the striking plate has a thickness in the
range of 0.060 to 0.0110.
- 15 4. The golf club head according to claim 1 wherein the striking plate is composed
of a material selected from the group consisting of titanium, titanium alloys, steels,
vitreous metals, ceramics, composites, carbon materials, carbon fiber materials, other
fibrous materials and mixtures thereof.
- 20 5. The golf club according to claim 1 wherein the striking plate has a durability to
withstand 2500 impacts with an USGA conforming golf ball at 110 miles per hour.

6. The golf club according to claim 1 wherein the striking plate has concentric regions of varying thickness with the thickest region in the center.

7. The golf club head according to claim 1 wherein the striking plate comprises a
5 central circular region having a base thickness, a first concentric region having a first thickness wherein the base thickness is greater than the first thickness, a second concentric region having a second thickness wherein the first thickness is greater than
the second thickness, a third concentric region having a third thickness wherein the second thickness is greater than the third thickness, and a periphery region having a
10 fourth thickness wherein the fourth thickness is less than the third thickness.

8. The golf club head according to claim 1 further comprising a face member comprising the striking plate and a face extension extending laterally inward from a perimeter of the striking plate, and an interior tubing for receiving a shaft, the interior
15 tubing engaging an upper portion of the face extension and a lower portion of the face extension.

9. The golf club head according to claim 1 wherein the golf club head has a coefficient of restitution of from 0.85 to 0.93.

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10. A golf club head comprising:

a face member comprising a face plate for striking a golf ball having an exterior surface and an interior surface, the face plate extending from a heel section of

5 the golf club head to a toe section of the golf club head, a face extension extending laterally inward from a perimeter of the face plate, and an interior tubing for receiving a shaft, the interior tubing engaging an upper portion of the face extension and a lower portion of the face extension;

a crown secured to the upper portion of the face extension at a
10 predetermined distance from the face plate; and

a sole plate secured to the lower portion of the face extension at a predetermined distance from the face plate.

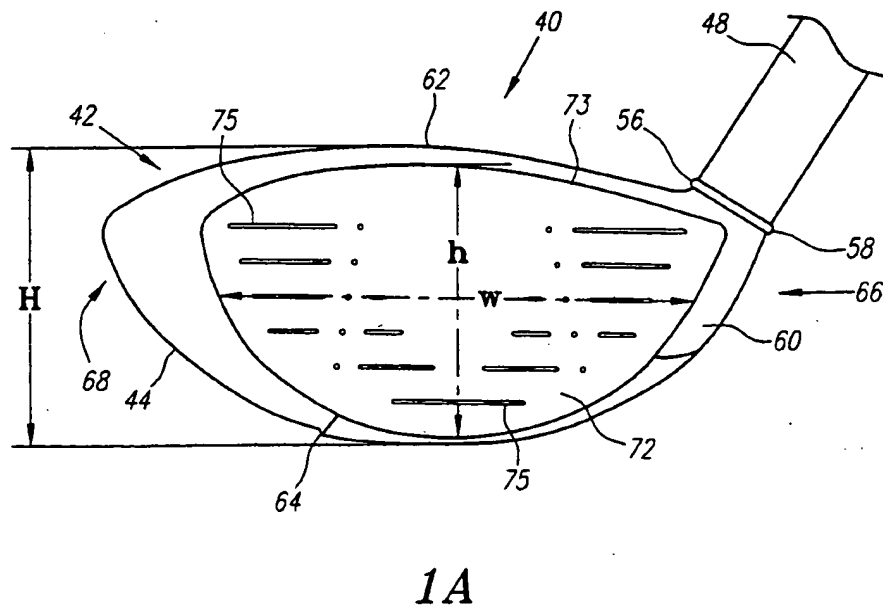
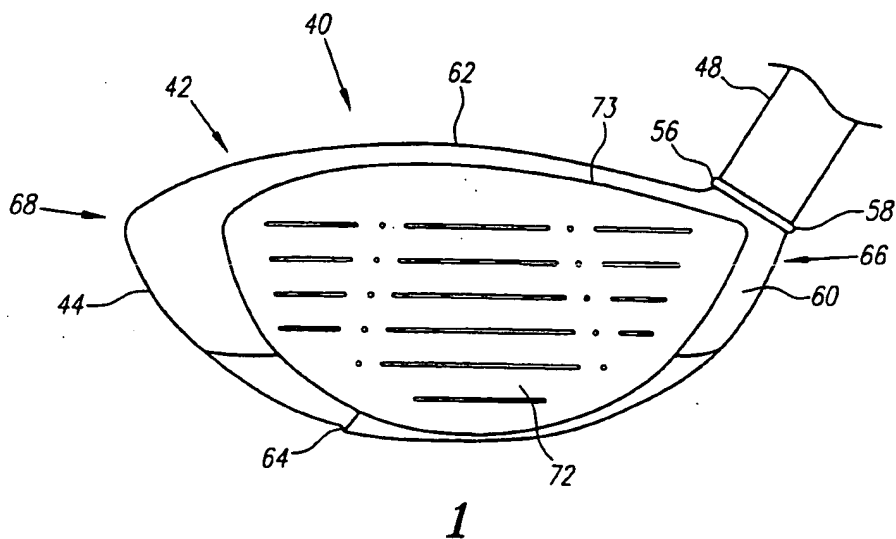
11. The golf club head according to claim 10 wherein the sole plate has ribbon
15 section that is secured to the crown.

12. The golf club head according to claim 10 wherein the face plate is composed of a forged titanium material.

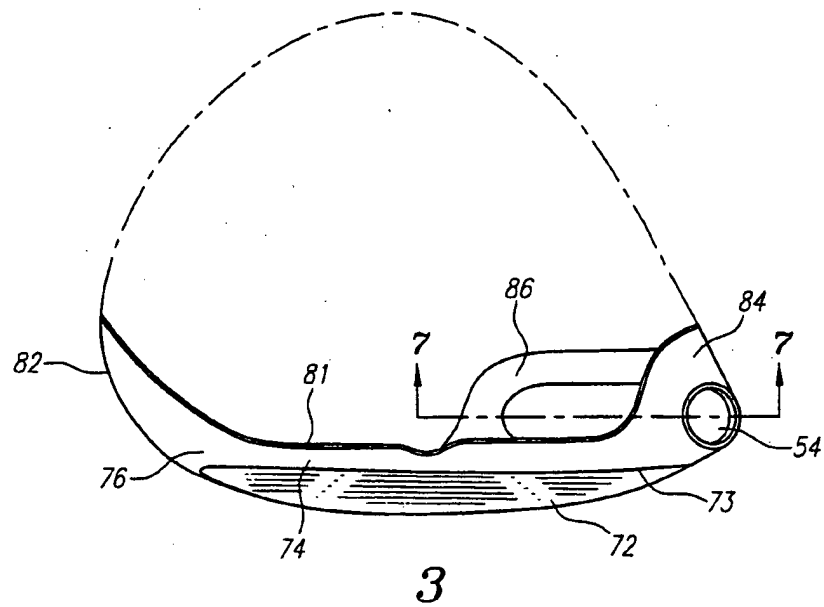
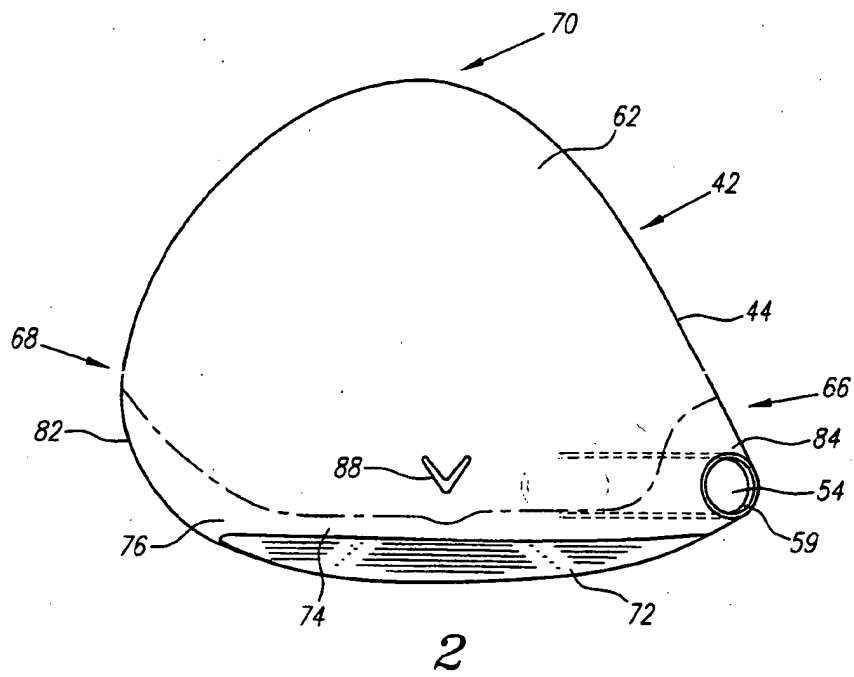
13. The golf club head according to claim 10 wherein the sole plate further comprises a medial ridge extending from the face section rearward and dividing the sole plate into a toe section and a heel section.
- 5 14. The golf club head according to claim 10 wherein the face plate of the face member has a thickness in the range of 0.010 inches to 0.250 inches, and has a coefficient of restitution of at least 0.83.
- 10 15. The golf club head according to claim 14 wherein the face plate has an aspect ratio no greater than 1.7.
16. The golf club head according to claim 10 wherein the thickness of face plate varies outward from a center of the face plate.
- 15 17. The golf club head according to claim 10 wherein the face plate has concentric regions of varying thickness with the thickest region in the center.

18. The golf club head according to claim 10 wherein the face plate comprises a central circular region having a base thickness, a first concentric region having a first thickness wherein the base thickness is greater than the first thickness, a second concentric region having a second thickness wherein the first thickness is greater than the second thickness, a third concentric region having a third thickness wherein the second thickness is greater than the third thickness, and a periphery region having a fourth thickness wherein the fourth thickness is less than the third thickness.
19. The golf club head according to claim 10 wherein the upper portion of the face extension has a hosel section extending about the interior tubing, the hosel section having a width greater than the entirety of the upper portion of the face extension.
20. The golf club head according to claim 10 wherein the lower portion of the face extension has a bore section extending about the interior tubing, the bore section having a width greater than the entirety of the lower portion of the face extension.

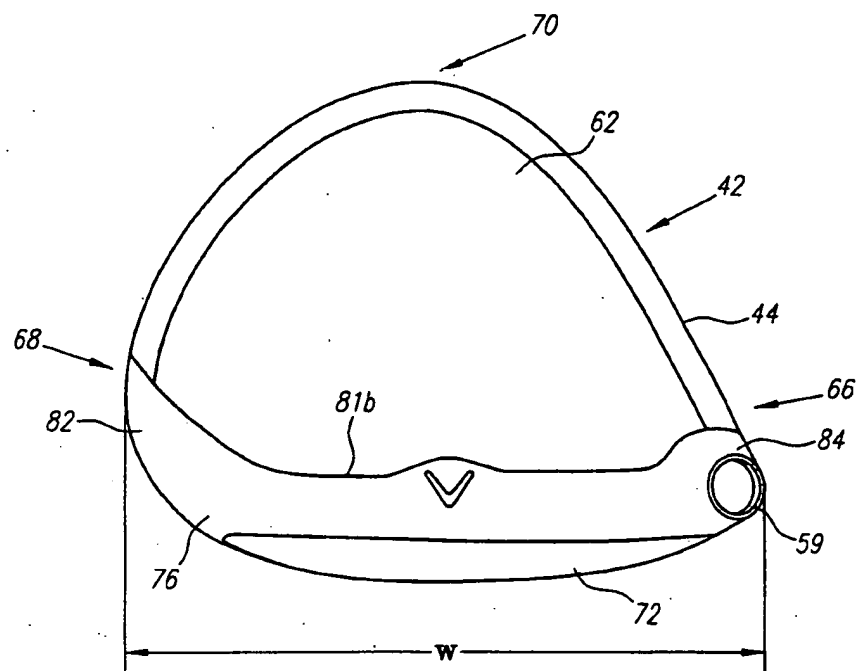
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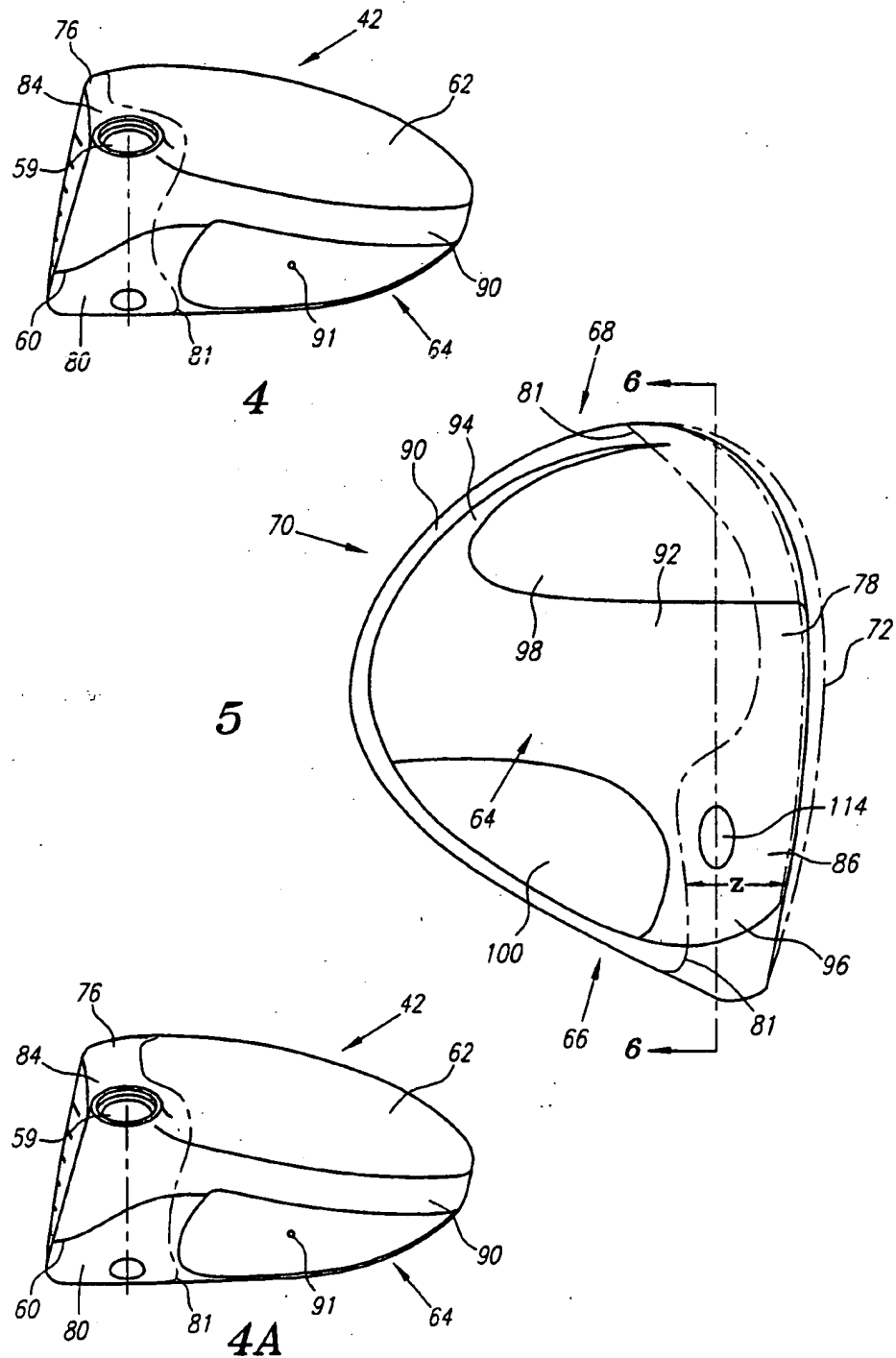


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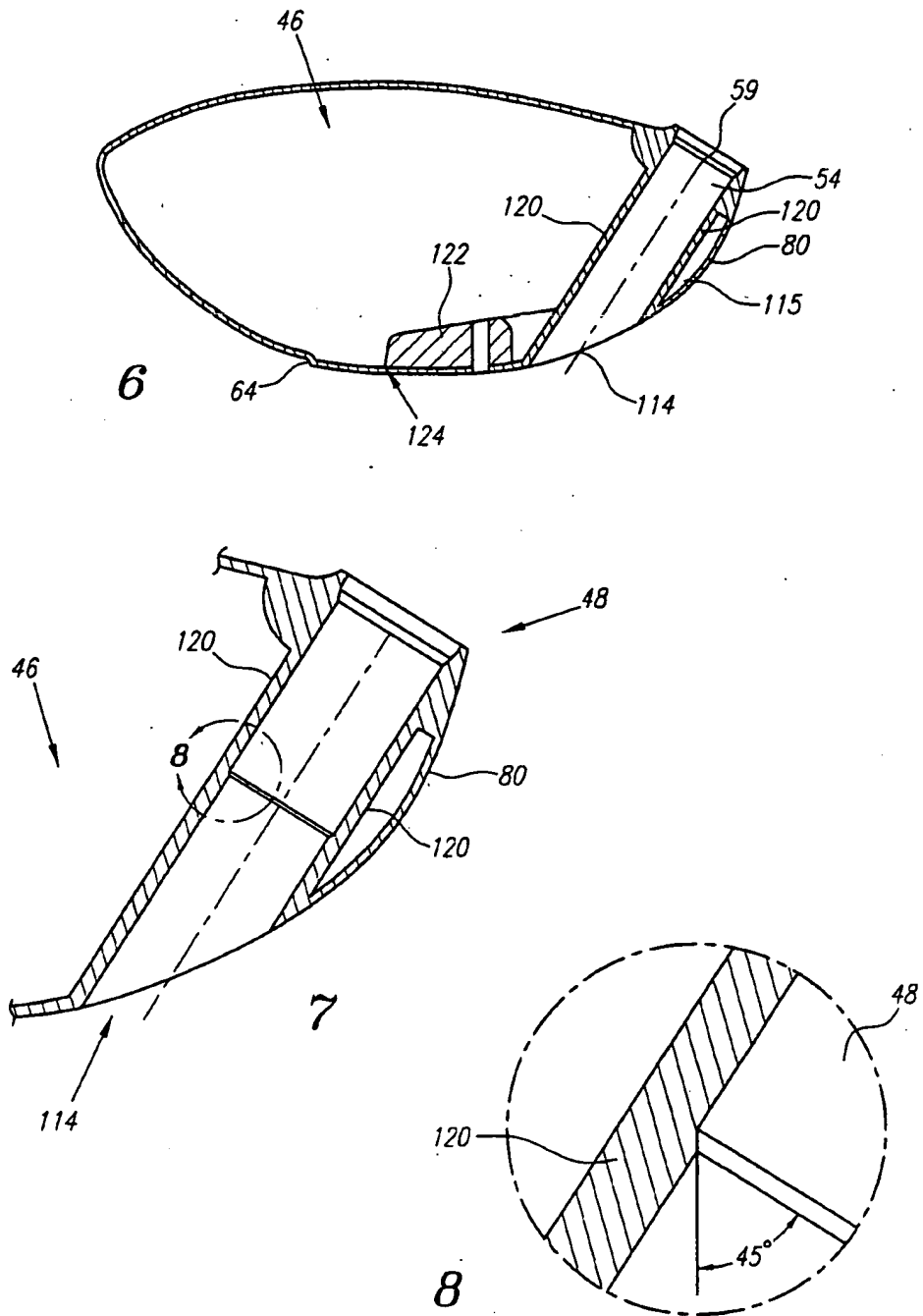


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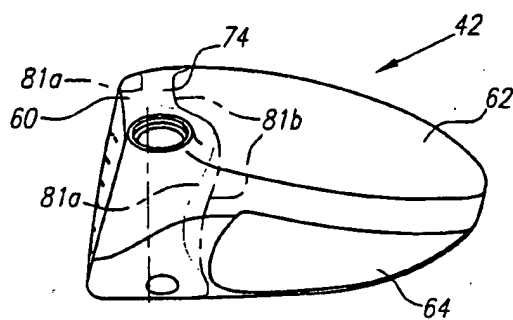
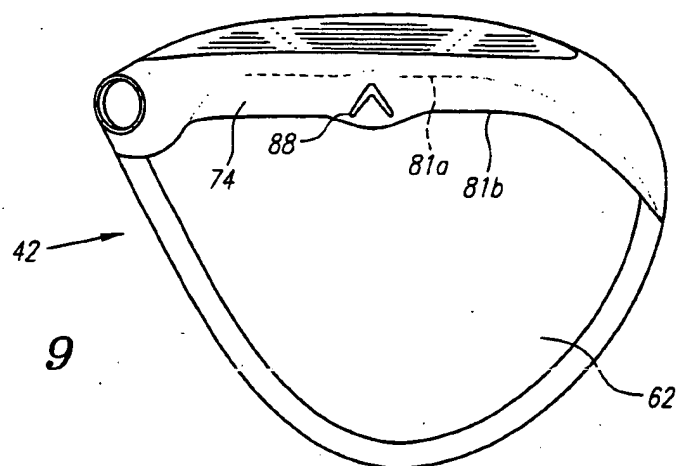
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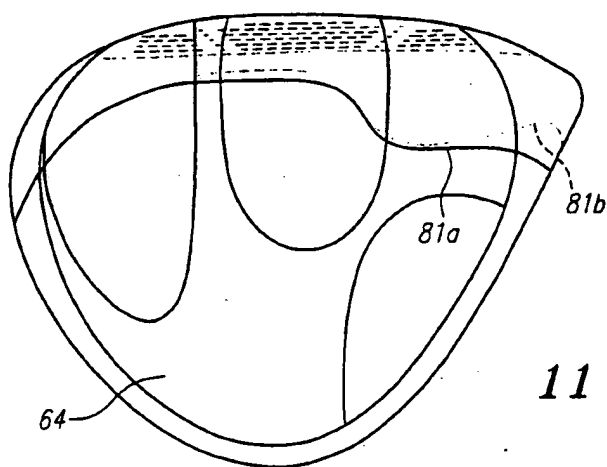
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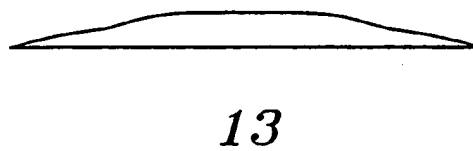
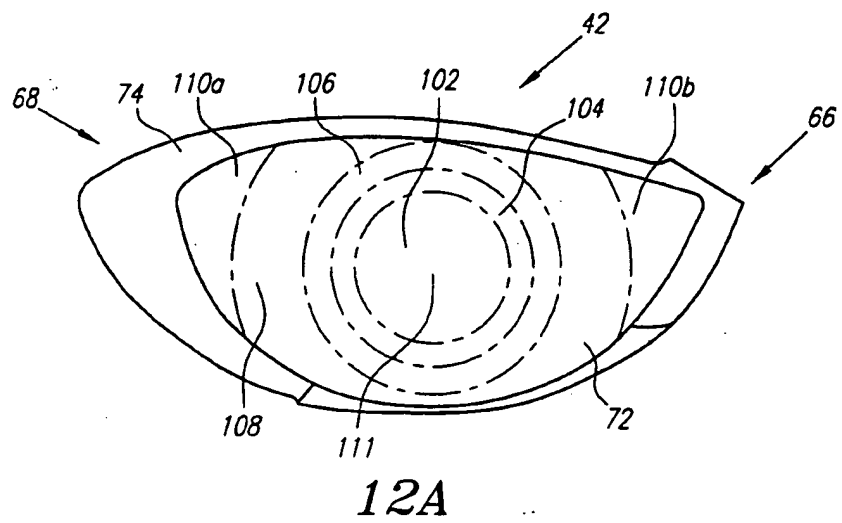
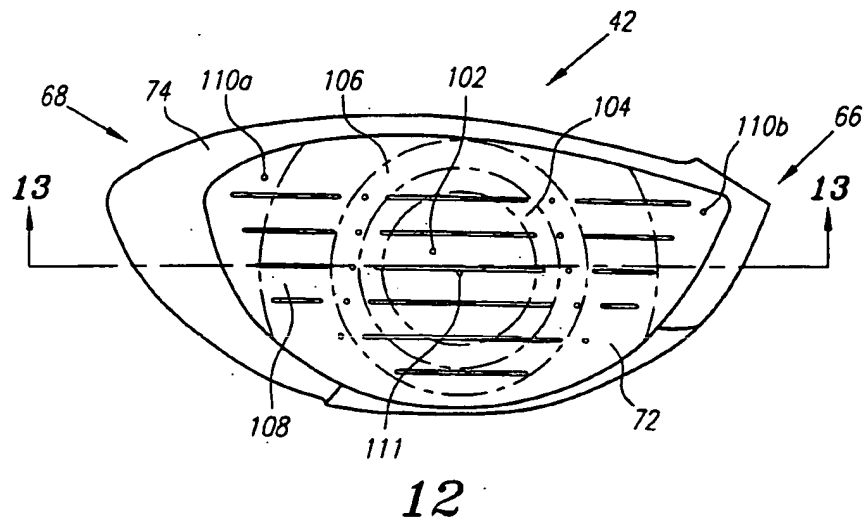


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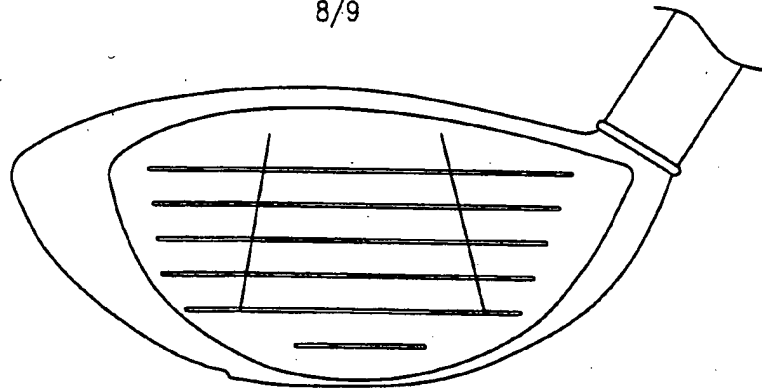


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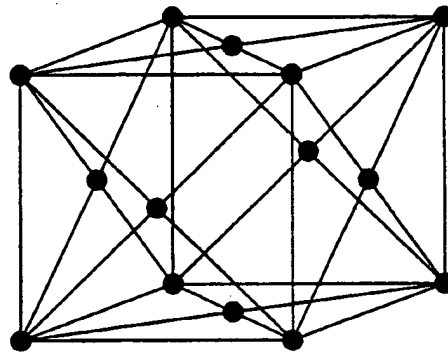
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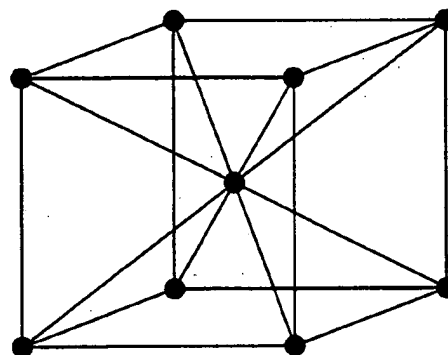
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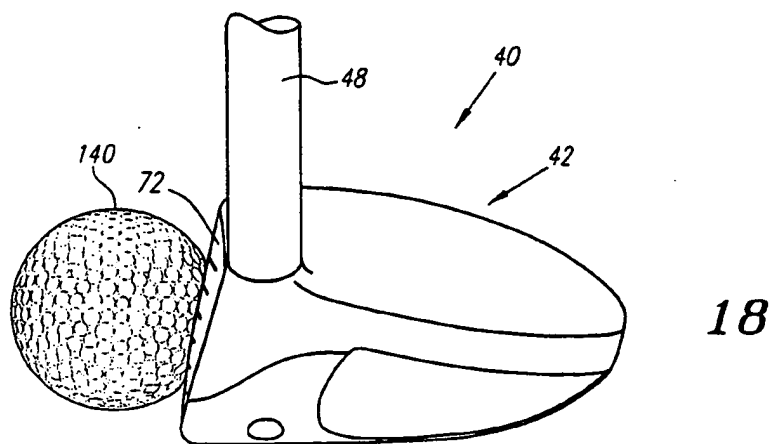
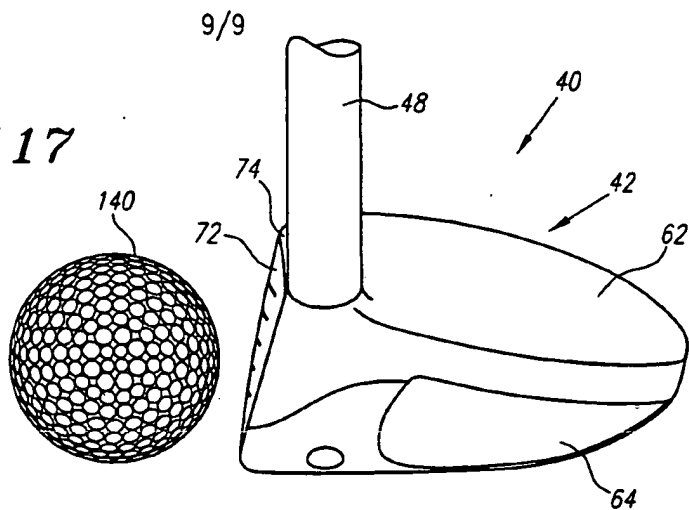
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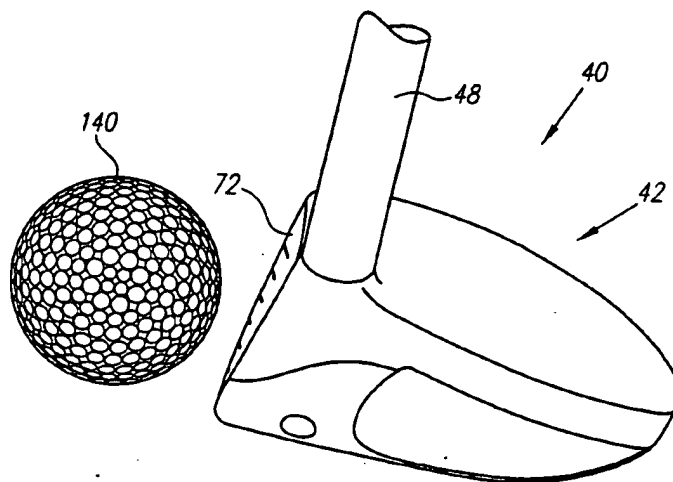
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INTERNATIONAL SEARCH REPORT

International application No.
PCT/US00/30103

A. CLASSIFICATION OF SUBJECT MATTER IPC(7) : A63B 53/04, 53/06 US CL : 473/329, 345 According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) U.S. : 473/329, 345, 324 Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) EAST/WEST		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5,830,084 A (<i>KOSMATKA</i>) 03 November 1998, See col. 5, lines 25-67.	1-20
X	US 5,474,296 A (<i>SCHMIDT et al.</i>) 12 December 1995, See col. 9, lines 1-57.	1-9
Y	US 5,094,383 A (<i>ANDERSON et al.</i>) 10 March 1992, See col. 3, line 5- col. 4, line 45.	1-20
Y	US 5,674,132 A (<i>FISHER</i>) 07 October 1997, See col. 8, lines 1-67.	1-20
Y	US 5,255,918 A (<i>ANDERSON et al.</i>) 26 October 1993, See col. 3, line 5- col. 4, line 44.	1-20
Y	US Re. 35,955 E (<i>LU</i>) 10 November 1998, See col. 5, lines 1-65.	1-20
<input type="checkbox"/> Further documents are listed in the continuation of Box C. <input type="checkbox"/> See patent family annex.		
* Special categories of cited documents: "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier document published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "Z" document member of the same patent family		
Date of the actual completion of the international search 11 DECEMBER 2000		Date of mailing of the international search report 16 JAN 2001
Name and mailing address of the ISA/US Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231 Facsimile No. (703) 305-3230		Authorized officer SNEH VARMA Telephone No. (703) 308-8335 <i>Sheila Varma</i> <i>Patent Specialist</i> <i>Technology Center 3700</i>

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